Problem 1.1

(a)

Derive an expression for the dimensionless cylinder volume $V(\theta)/V(0) = f(\theta, r, \varepsilon = s/2l)$

Solution:

From Figure 1.1, and using trig relations, we have

The instantaneous stroke is $y = l + a - [(l^2 - a^2 \sin^2 \theta)^{1/2} + a \cos \theta]$ The instantaneous volume is $V(\theta) = V(0) + \pi/4 b^2 y$ The displacement volume is $V_d = \pi/4 b^2 s$ The stroke is s = 2aThe compression ratio is $r = (V(0) + V_d)/V(0) = 1 + V_d/V(0) \Rightarrow V_d = (r-1) V(0)$

Therefore, $\pi/4 \ b^2 = V_d/s = (r-1) \ V(0)/s$ and $V(\theta) = V(0) + (r-1) \ V(0)y/s$

so

$$V(\theta)/V(0) = 1 + (r-1) (l + a - [(l^2 - a^2 \sin^2 \theta)^{1/2} + a \cos \theta])$$

= 1 + (r-1) l [1 + a/l - (1 - (a/l)^2 \sin^2 \theta)^{1/2} - a/l \cos \theta])/s
= 1 + (r-1) l [1 + \varepsilon - (1 - \varepsilon^2 \varepsilon \varepsilon^{1/2} - \varepsilon \cos \varepsilon])/2\varepsilon

(b) The plot of dimensionless cylinder volume for r = 10, s = 100 mm and l = 150 mm is shown below:



Problem 1.2

(a)

Derive an expression for the dimensionless piston speed.

Solution:

The instantaneous piston speed is $U_p = dy/dt = dy/d\theta * d\theta/dt$

The instantaneous stroke is
$$y = l + a - [(l^2 - a^2 \sin^2 \theta)^{1/2} + a \cos \theta]$$

differentiating y with respect to crank angle θ , we have

$$\frac{dy}{d\theta} = -\left[\frac{1}{2}\left(l^2 - a^2\sin^2\theta\right) - \frac{1}{2}\left(-2a^2\sin\theta\cos\theta\right) - a\sin\theta\right]$$
$$= +a\sin\theta\left[1 + \cos\theta\left[\left(l/a\right)^2 - \sin^2\theta\right]^{1/2}\right]$$

The angular velocity is $d\theta/dt \ (rad/time) = N \ (rev/time) \ 2\pi \ (rad/rev)$

The mean piston speed is $\underline{U}_p = 2Ns = 4Na$

The ratio of the instantaneous piston speed to the mean piston speed is therefore:

$$U_p(\theta)/\underline{U}_p = 2\pi N \, a \, \sin\theta \, [1 + \cos\theta / [(l/a)^2 - \sin^2\theta]^{1/2} \,]/ \, 4Na$$
$$= \pi/2 \, \sin\theta \, [1 + \cos\theta / [(l/a)^2 - \sin^2\theta]^{1/2} \,]$$

(b) The plot of dimensionless piston speed for s = 100 mm and l = 150 mm is shown below:



Problem 1-3

Find the ratio of the initial to final swirl speed as f (r, geometry) for a cylinder with a dished piston. The cylinder bore is b, and the diameter of the piston dish is d. The angular velocity distribution is equivalent to solid body rotation.

Solution:

At bottom dead center (1), the moment of inertia is $I_1 = \pi \rho_1 (b^4 s + d^4 h)/32$ At top dead center (0), the moment of inertia is $I_o = \pi \rho_o d^4 h/32$

If angular momentum is conserved, then $I_I \omega_I = I_o \omega_o$ so the ratio of the initial to final swirl speeds is $\omega_o / \omega_I = I_I / I_o = \rho_I / \rho_o [(b^4 s + d^4 h) / d^4 h]$

We now need to express the density ratio as a function of cylinder geometry. The gas density increases with cylinder compression. Since the amount of gas in the cylinder is constant,

$$\rho_l/\rho_o = V_o/V_l = l/r$$

so

$$\omega_{o} / \omega_{l} = 1/r(b^{4}s + d^{4}h)/d^{4}h] = 1/r [(b/d)^{4} s/h + 1]$$

we can simplify this by expressing the stroke in terms of the other variables

Since

$$r = V_l/V_o = (b^2 s + d^2 h)/d^2 h$$

then $s/h = (r-1)d^2/b^2$

and in final form, the swirl speed ratio is

$$\omega_o / \omega_l = (b/d)^2 (r-1)/r + 1/r$$

For r >> 1, the swirl increases quadratically with diameter ratio.

Problem 1-4

Determine how the power/weight = f(number of cylinders keeping V_d constant) assuming mep, mean piston speed, mass/ displacement volume, and Power/area are not a function of V_d , and equal bore and stroke.

Solution:

The power/weight can be expanded in terms of the power/area and mass/ displacement volume as

$$\frac{\dot{W}}{m} = \frac{\frac{\dot{W}}{A}\frac{\pi}{4}b^2n_c}{\frac{m}{V_d}\frac{\pi}{4}b^2sn_c}$$

If b = s, then $V_d = \pi/4 b^3 n_c$, and

$$b = \left(\frac{4 V_d}{\pi nc}\right)^{1/3}$$

and
$$\frac{\dot{W}}{m} = \frac{\frac{\dot{W}}{A}}{\frac{\dot{M}}{V_d}} \left(\frac{\pi n_c}{4 V_d}\right)^{1/3} \approx n_c^{1/3}$$

The power per unit weight scales as the number of cylinders to the 1/3 power.

Problem 1-5

Compute the mean piston speed, bmep, torque, and power/area for three engines, 1: Marine, 2: Dragster, and 3: Formula One.

Solution:

a) Mean Piston Speed

$$\overline{U}_{p} = 2 N s$$

$$1: \overline{U}_{p} = 2 \cdot 2600 \frac{rev}{\min} \cdot \frac{\min}{60s} \cdot 0.127 = 11.0 m/s$$

$$2: \overline{U}_{p} = 2 \cdot 6400 \frac{rev}{\min} \cdot \frac{\min}{60s} \cdot 0.095 = 20.3 m/s$$

$$3: \overline{U}_{p} = 2 \cdot 10500 \frac{rev}{\min} \cdot \frac{\min}{60s} \cdot 0.057 = 19.95 m/s$$

b) bmep (assuming all are four stroke engines)

$$bmep = \frac{2 \dot{W}_b}{V_d N}$$
1: $bmep = \frac{2 \cdot 1118}{12 \cdot \frac{\pi}{4} \cdot 0.136^2 \cdot 0.127 \cdot \frac{2600}{60}} = 2.33 \ x 10^3 \ kPa = 23.3 \ bmep$
2: $bmep = \frac{2 \cdot 447}{8 \cdot \frac{\pi}{4} \cdot 0.108^2 \cdot 0.095 \cdot \frac{6400}{60}} = 1.20 \ x 10^3 \ kPa = 12.0 \ bar$
3: $bmep = \frac{2 \cdot 522}{8 \cdot \frac{\pi}{4} \cdot 0.086^2 \cdot 0.057 \cdot \frac{10500}{60}} = 2.25 \ x 10^3 \ kPa = 22.5 \ bar$

Problem 1-5 (cont) c) torque

$$\tau = \frac{\dot{W}}{2 \pi N}$$

$$1: \tau = \frac{(1118 \times 10^3)}{2\pi \cdot \frac{2600}{60}} \frac{W}{rev} = 4106 Nm$$

$$2: \tau = \frac{(447 \times 10^3)}{2\pi \cdot \frac{6400}{60}} = 667 Nm$$

$$3: \tau = \frac{(522 \times 10^3)}{2\pi \cdot \frac{10500}{60}} = 475 Nm$$

d) power/piston area

$$\frac{\dot{W}}{A_p} = \frac{\dot{W}}{\frac{\pi}{4}b^2 n_c}$$

$$1: \frac{\dot{W}}{A_p} = \frac{1118}{12 \cdot \frac{\pi}{4} \cdot 0.136^2} = 6413 \, kW \, / \, m^2$$

$$2: \frac{\dot{W}}{A_p} = \frac{447}{8 \cdot \frac{\pi}{4} \cdot 0.108^2} = 6099 \, kW \, / \, m^2$$

$$3: \frac{\dot{W}}{A_p} = \frac{522}{8 \cdot \frac{\pi}{4} \cdot 0.086^2} = 11,233 \, kW \, / \, m^2$$

Problem 1-6

Compute the air flow rate, given e_v , ρ_i , V_d , N, for the marine engine given in Problem 1-5.

Solution:

Assuming that the engine is a four stroke fuel injected engine, then

$$\dot{m}_{a} = \frac{1}{2} e_{v} \rho_{i} V_{d} N$$
$$= \frac{1}{2} \cdot 0.8 \cdot 1.5 \cdot 1.17 \cdot 0.0221 \cdot \frac{2600}{60}$$
$$= 0.67 \ kg \ / \ s$$

Problem 1-7

Find the bmep, efficiency, and air/fuel ratio of an engine, given V_d , power, N, e_v , bsfc, and q_c .

Solution:

At 298 K and 1 bar, assume the gas density is 1.17 kg/m^3

$$bmep = \frac{2\dot{W}}{V_d N} = \frac{2 \cdot 88}{3.8 \times 10^{-3} \cdot \frac{4000}{60}} = 694 \, kPa$$

$$\eta = \frac{1}{bsfc \cdot q_c} = \frac{1}{0.35 \cdot \frac{42000}{3600}} = 0.24$$

$$\dot{m}_f = \dot{W} \cdot bsfc = 88 \cdot \frac{0.35}{3600} = 8.55 \, x \, 10^{-3} \, kg \, / \, s$$

$$\dot{m}_a = \frac{1}{2} e_v \rho V_d N = \frac{1}{2} 0.85 \cdot 1.17 \cdot 3.8 \, x \, 10^{-3} \cdot \frac{4000}{60} = 0.125 \, kg \, / \, s$$

$$A = \frac{\dot{m}_a}{\dot{m}_f} = \frac{0.125}{8.55 \, x \, 10^{-3}} = 14.7$$

Problem 1-8

Find the bmep and mean piston speed of an engine, given n_c , τ , N, b, s

Solution:

$$bmep = \frac{2\pi\tau}{V_d} = \frac{2\pi \cdot 1100}{6 \cdot \frac{\pi}{4} \cdot 0.123^2 \cdot 0.127} = 7.63 \, x \, 10^5 \, N \, / \, m^2 = 7.63 \, bar$$

$$\overline{U}_p = 2Ns = 2 \cdot 2100 \cdot 0.127 \cdot \frac{1}{60} = 8.89 \, m/s$$

Problem 1-9

Compute the fuel/air ratio and the air flow rate for an engine given V_d , N, b, s, bmep, bsfc, and D_r .

Solution:

Assume $\rho_{amb} = 1.17 \text{ kg/m}^3$

$$F = \frac{\dot{m}_{f}}{\dot{m}_{a}}$$

$$bmep = \frac{\dot{W}_{b}}{V_{d} N}$$

$$bsfc = \frac{\dot{m}_{f}}{\dot{W}_{b}}$$

$$\therefore \quad \dot{m}_{f} = bmep \cdot bsfc \cdot V_{d} \cdot N$$

$$= 6.81 \times 10^{5} \cdot \frac{0.49}{3600} \cdot \frac{\pi}{4} \cdot 0.082^{2} \cdot 0.072 \cdot \frac{5500}{60} = 3.23 g/s$$

$$\dot{m}_{a} = D_{r} \cdot \rho_{amb} \cdot V_{d} N$$

$$= 0.748 \cdot 1.17 \cdot 3.8 \times 10^{-4} \cdot \frac{5500}{60} = 3.048 \times 10^{-2} kg/s = 30.48 g/s$$

$$F = \frac{3.23}{30.48} = 0.106$$